

Altair Inspire 를 활용한 자작자동차 부품 최적설계.

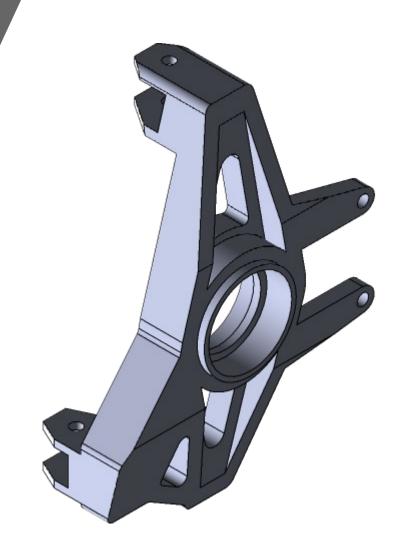
한양대학교 자작자동차동아리 팀 RACE -김범수, 민동혁

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- 2. 서스펜션 벨 크랭크 최적설계

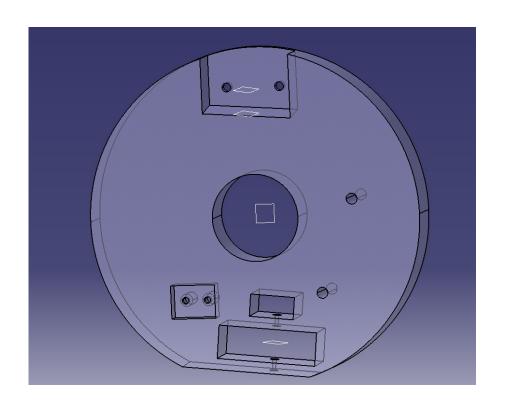
주제 선정 배경

2023 KSAE 대회를 위한 차량 설계 현가하질량의 감소를 통한 차량의 동적성능 향상 -> 너클 감량을 통한 현가하질량 최소화



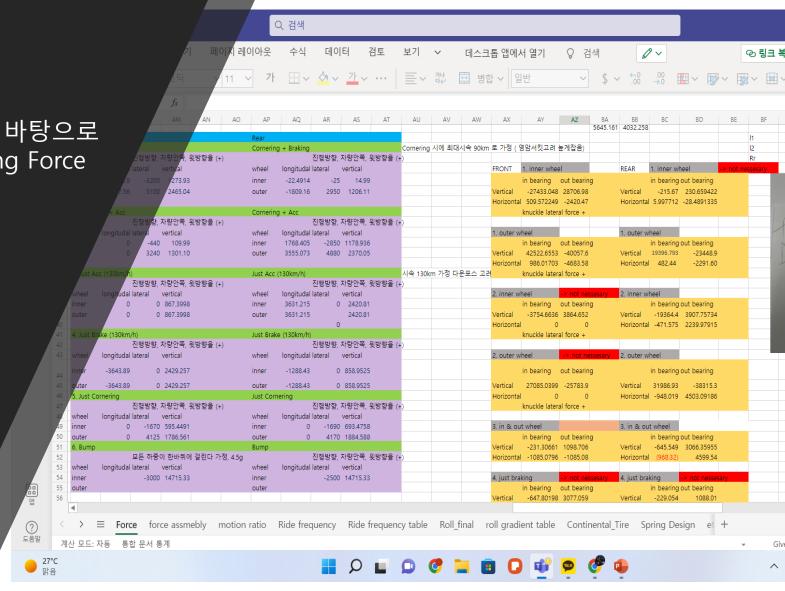
첫번째 디자인 스페이스

차량의 세팅값 설계에 맞게 볼트,너트등 과 간섭이 안나도록 디자인 스페이스 형상 설계

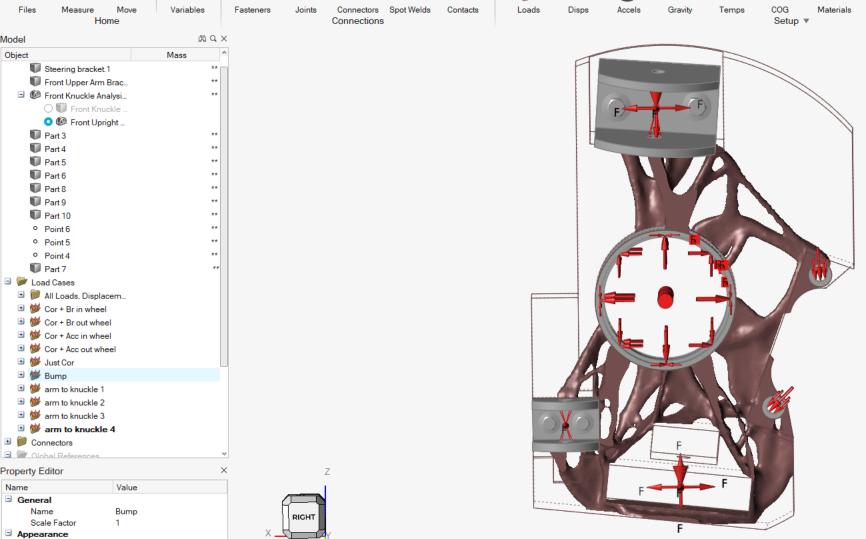


차량의 기본 설계 및 에어로 Down Force를 바탕으로 그 값들을 대입하여 너클에 가해지는 Bearing Force 및 각 상황들의 하중을 엑셀로 구현 함.

-> 이러한 Load Cases 를 바탕으로 Altair Inspire 의 Optimize 를 이용하여 최적설계 진행















Visible Behavior Current



































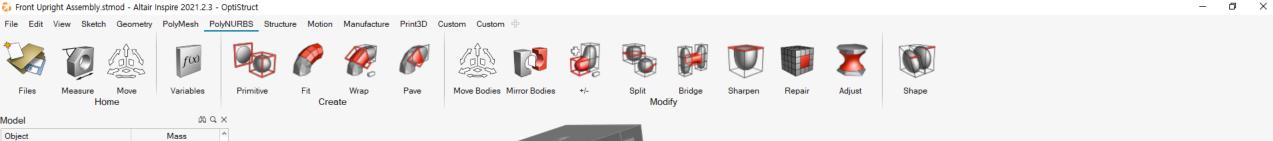


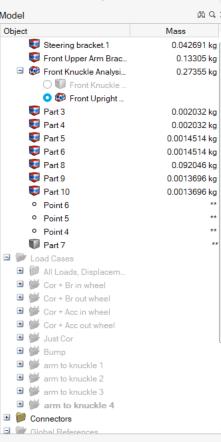


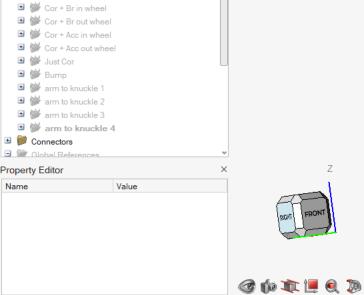
Shape Controls Bead Patterns

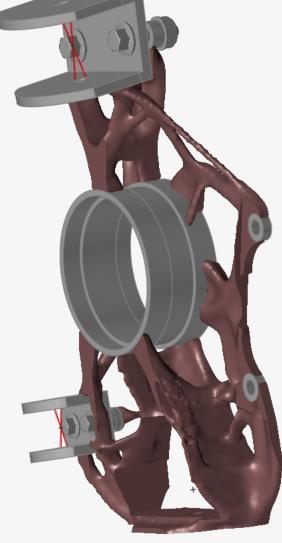
Analyze

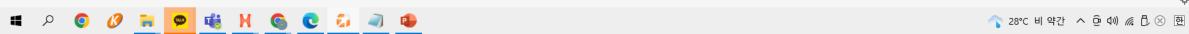
Systems

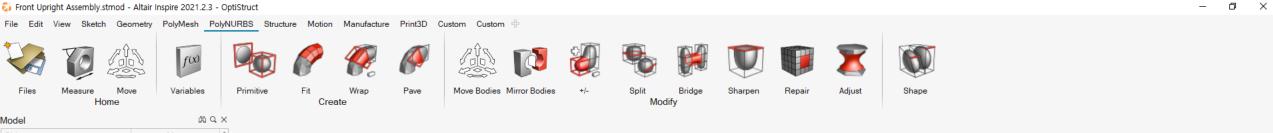


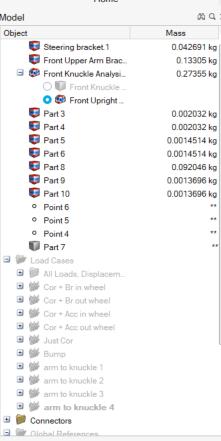


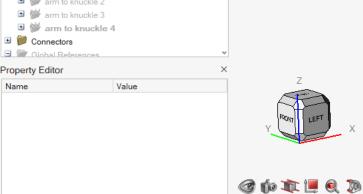


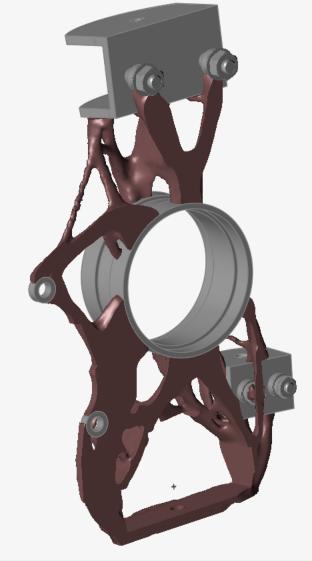








































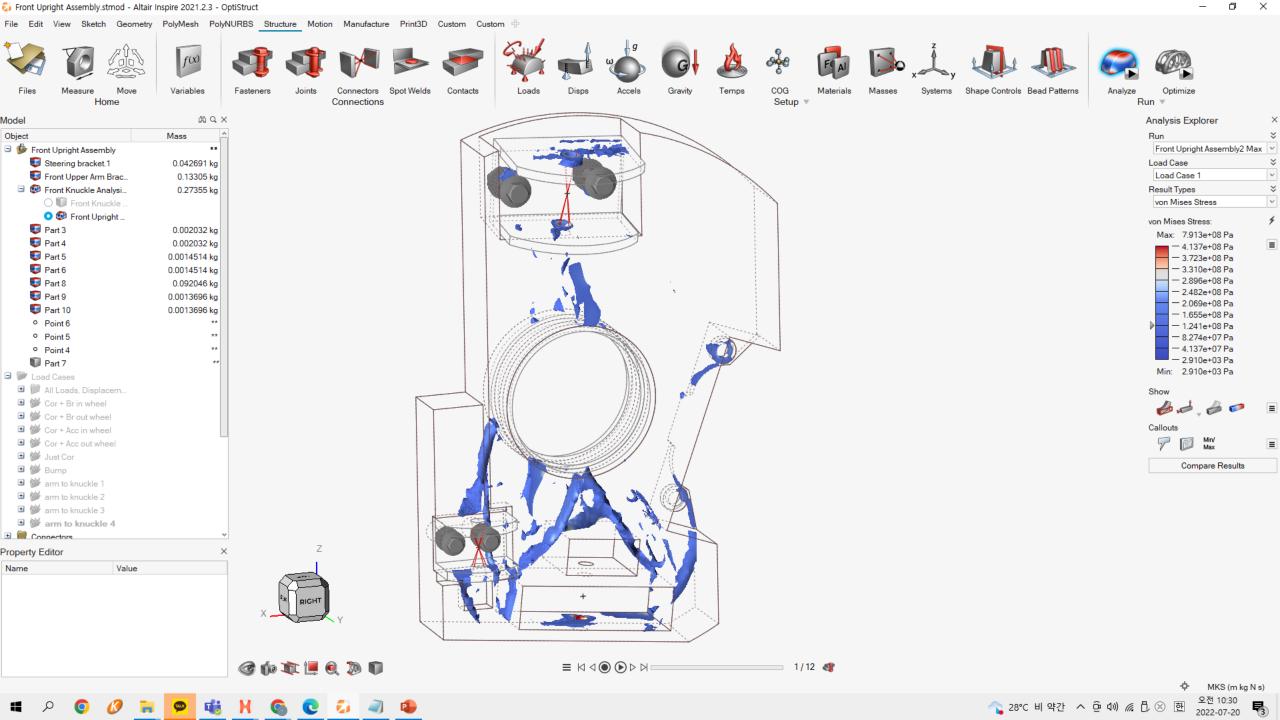


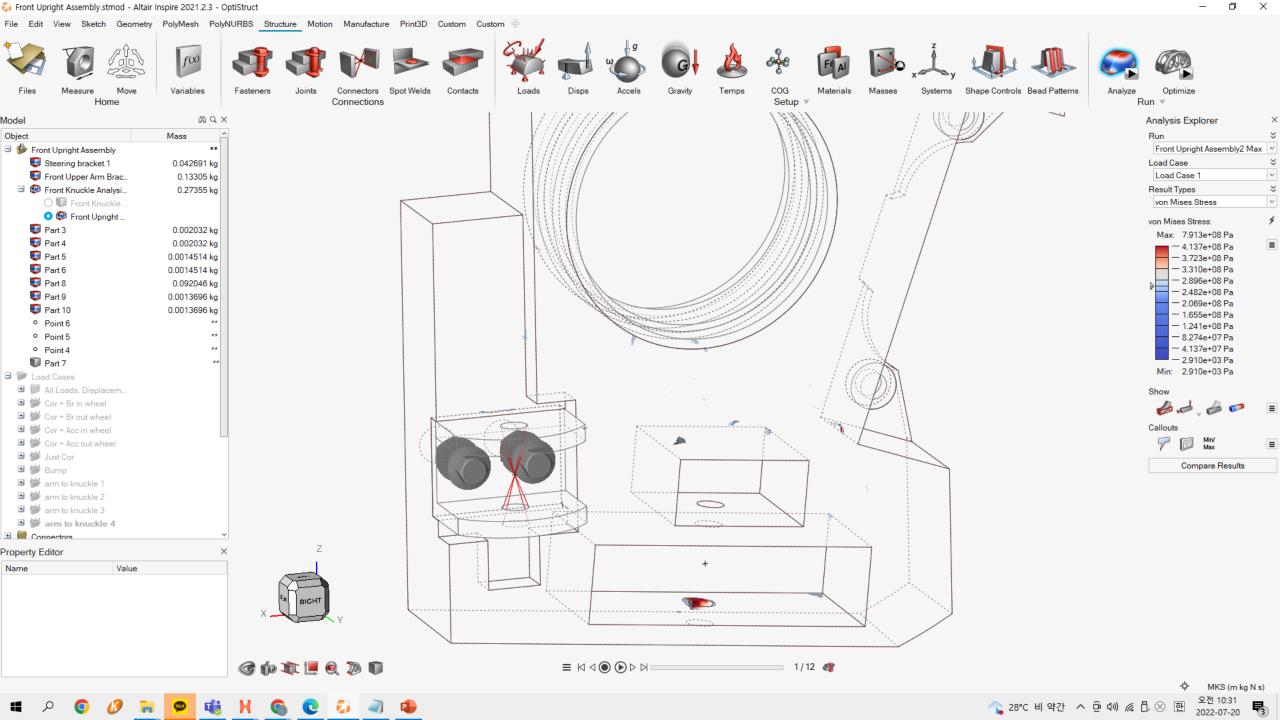






MKS (m kg N s)





메탈 3D프린팅 업체와 연락하여 무상 후원을 기대하고 Optimize 형상을 손보고 메탈 프린팅을 할 계획이었으나, 생각보다 비싼 가격으로 인하여 후원 협상이 무산되었다.

-> 3축 CNC 머신 가공이 용이하게 Inspire 의 Single draw 및 Extrusion 기능을 활용하여 다시 Topology 진행.



o × Model.stmod - Altair Inspire 2021.2.3 - OptiStruct File Edit View Sketch Geometry PolyMesh PolyNURBS Structure Motion Manufacture Print3D Custom Custom 🕆





















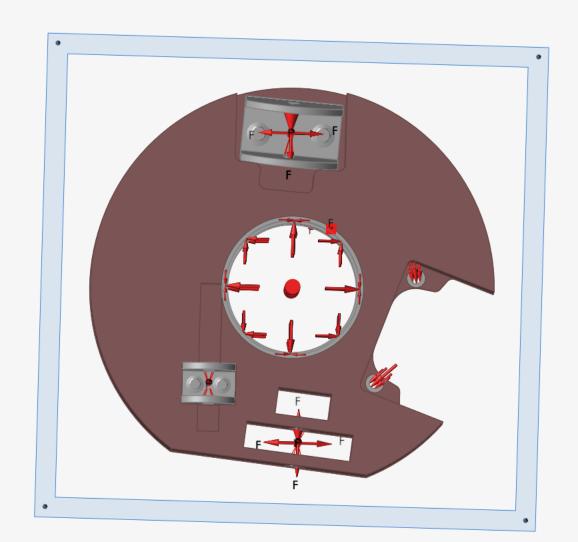








Analyze Run ▼







Property Editor Name

General

Name Behavior





Value

Front Knuckle Analy..

Move

Home

Steering bracket.1 Front Upper Arm Brac... Front Knuckle . O @ Front Upright ..

□ F All Loads, Displacem... Support 1 ▲ Support 2 Support 3 T Support 4 🖋 steering √ Force 4 √ Force 5 ✓ Force 6.

Part 1 Part 2 Part 3

Part 4 Part 5 Part 6 Part 7 Part 8 Part 9 O Point 1 Point 2 Point 3

Model Object □ 👺 Model Variables

角QX

**











@ fo it [Q D







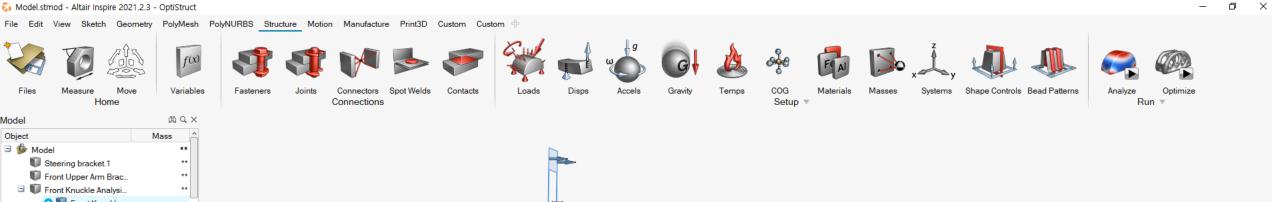


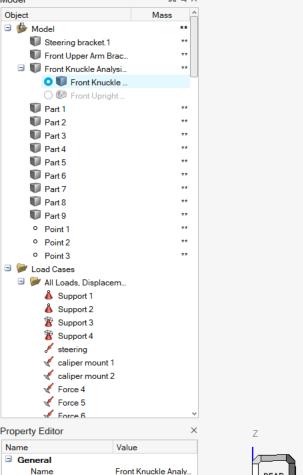


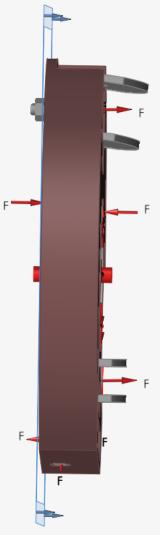




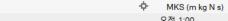
MKS (m kg N s)











Behavior

Active







~













@ fo it !! (Q)

REAR













o × Model.stmod - Altair Inspire 2021.2.3 - OptiStruct File Edit View Sketch Geometry PolyMesh PolyNURBS Structure Motion Manufacture Print3D Custom Custom 🕆









































Run ▼





Fasteners



















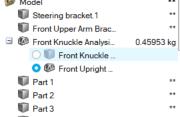
Systems

Shape Controls Bead Patterns

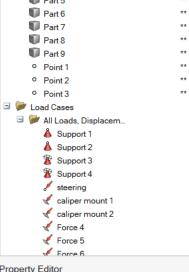
Analyze

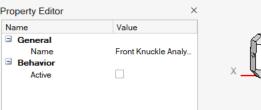


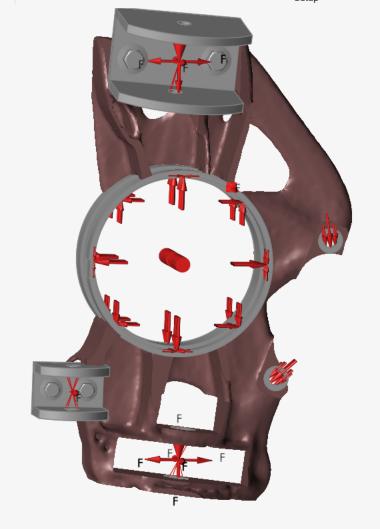
Home 角QX Model Object Mass □ 👺 Model Steering bracket.1































@ fo it [Q D



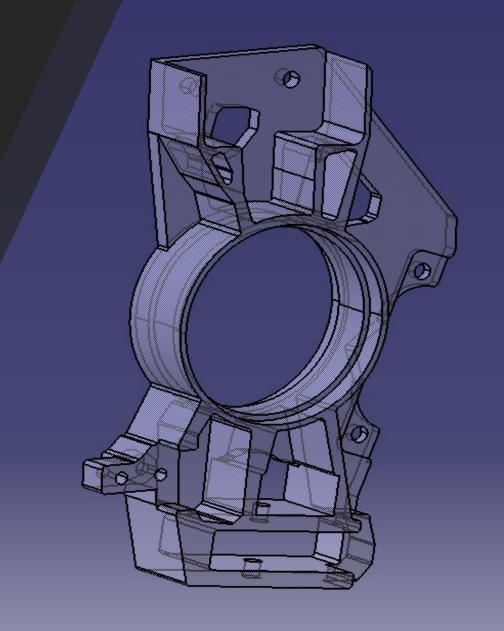


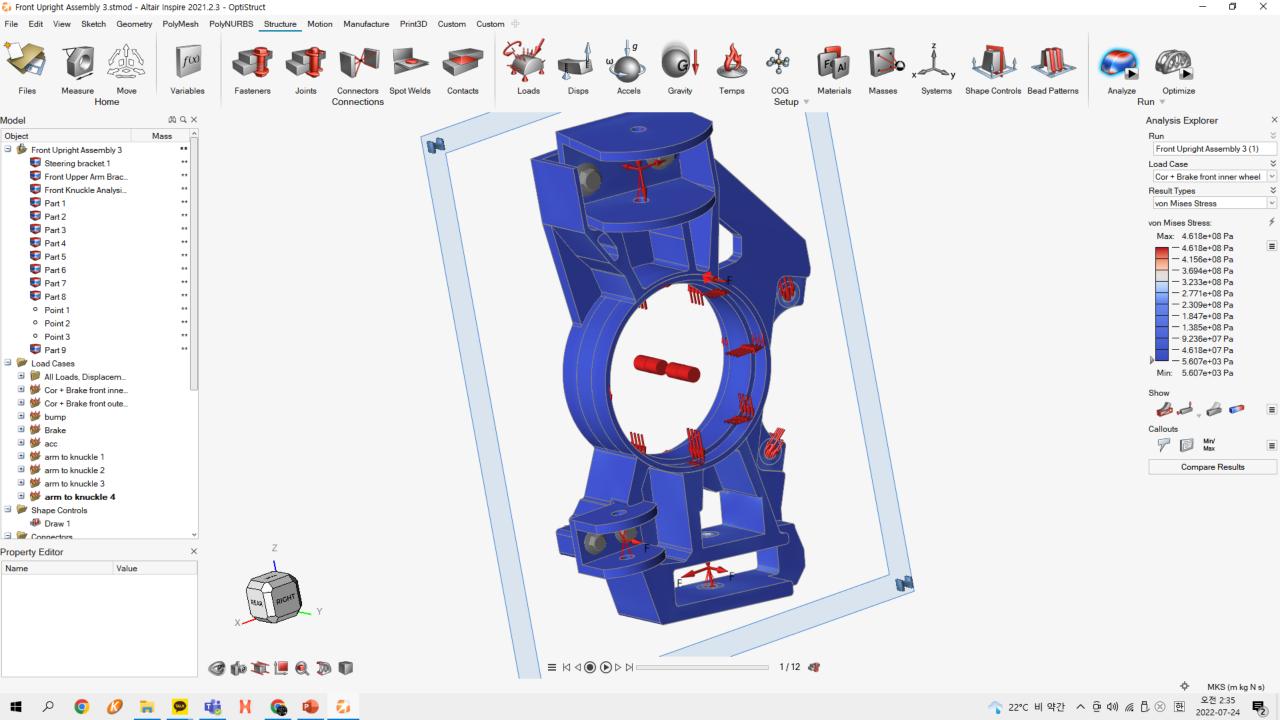


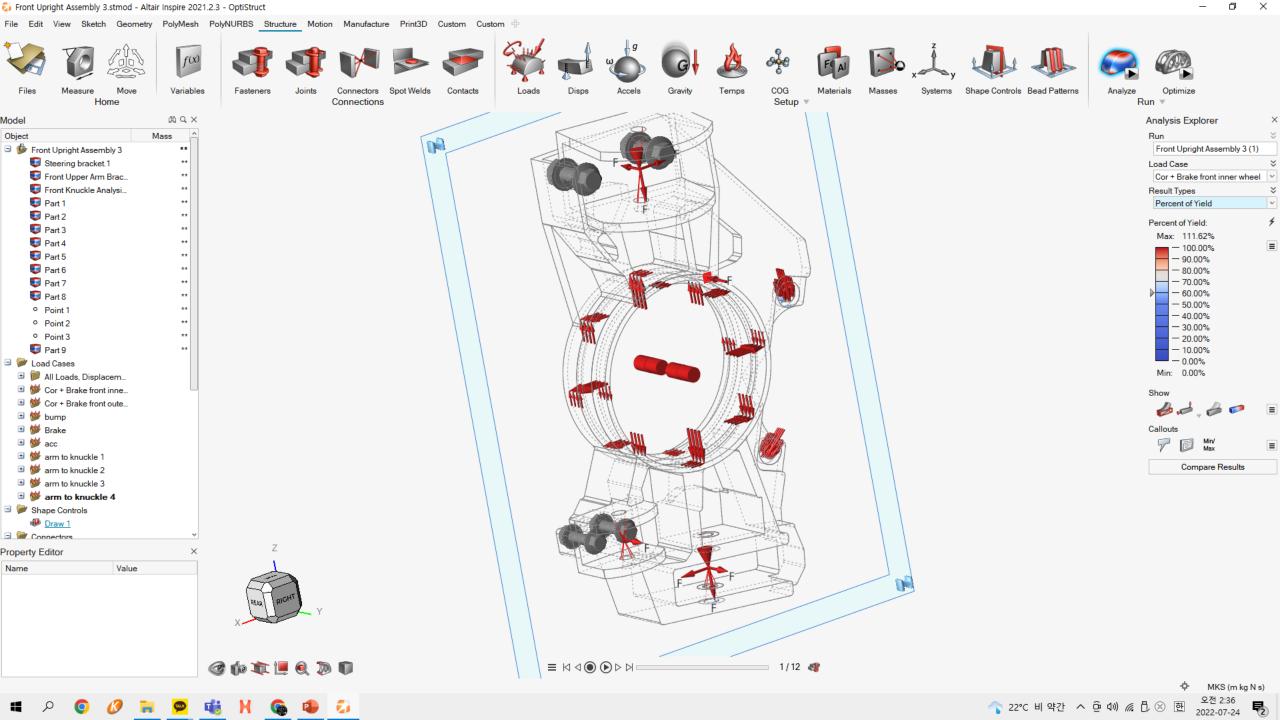


Single Draw Topology 형상을 통한 1차 살빼기

-> Analyze 진행



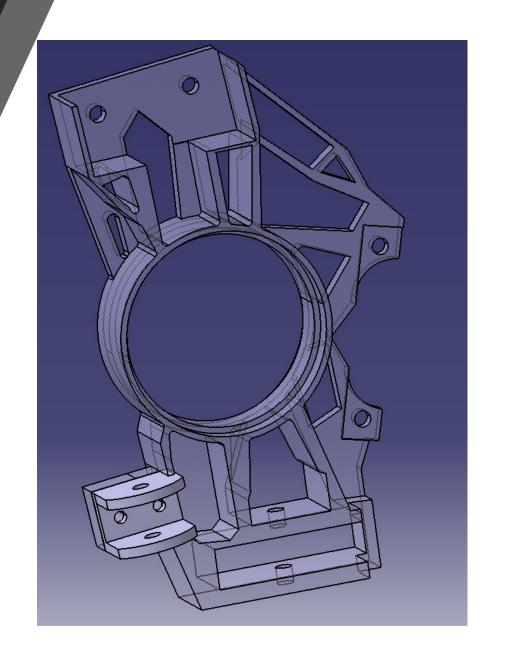




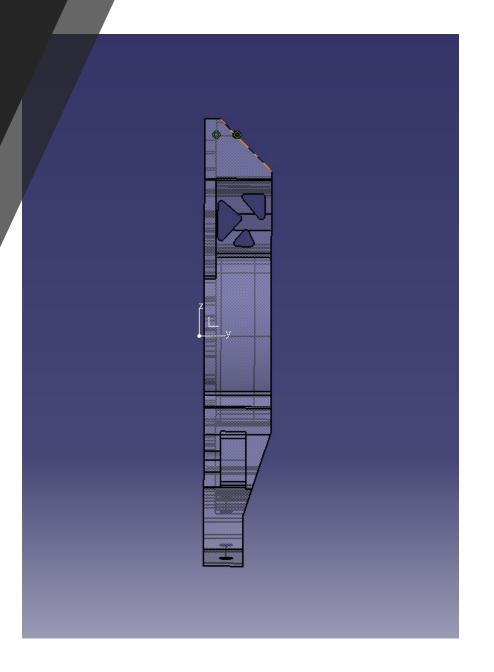
브레이크 캘리퍼 마운트 및 로워암 포인트에 응력이 집중, 그 부분의 두께를 늘림.

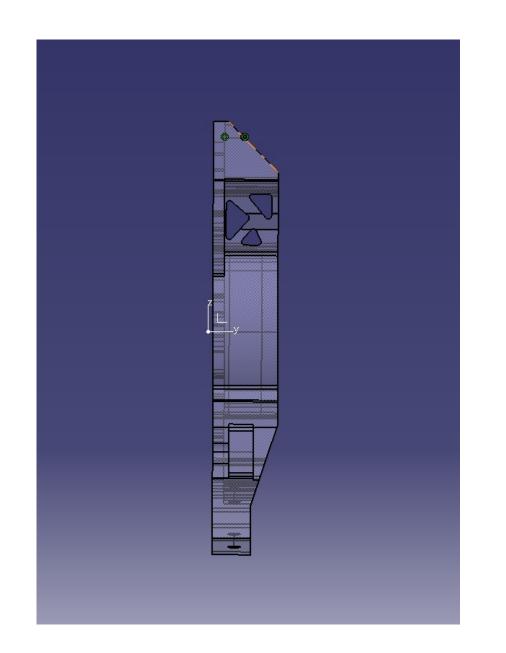
3축 CNC가공 용이하게 Extrusion의 조건을 주고 Topology를 진행.

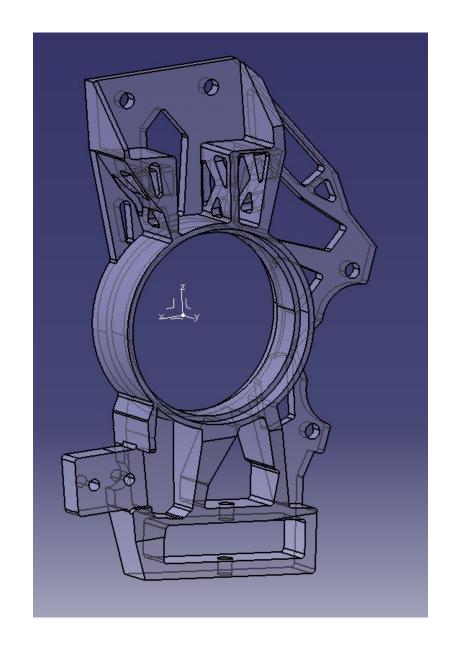
이를 바탕으로 2차 살빼기 진행. ->



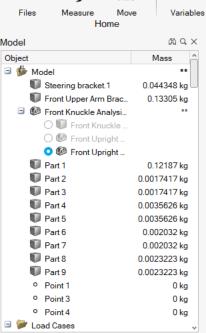
X축 방향으로의 살빼기를 위하여 Extrusion 조건을 주고 다시 3차 살빼기를 진행.

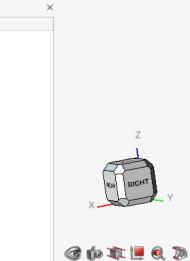






o × Model.stmod - Altair Inspire 2021.2.3 - OptiStruct File Edit View Sketch Geometry PolyMesh PolyNURBS Structure Motion Manufacture Print3D Custom Custom 🕆 f(x)





Fasteners







Property Editor Name





Value



























Connectors Spot Welds

Connections

Contacts





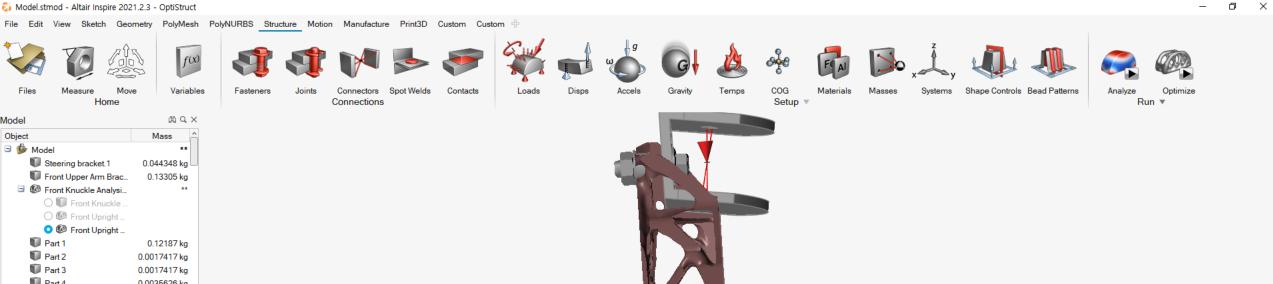


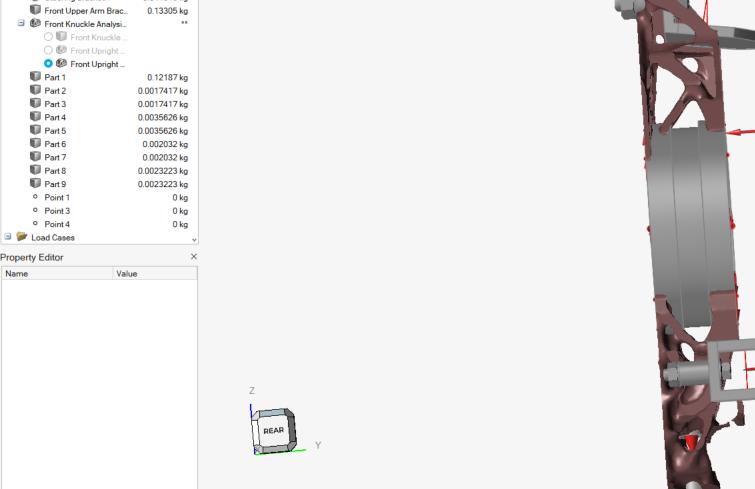
Systems Shape Controls Bead Patterns

Analyze

Run ▼

MKS (m kg N s)































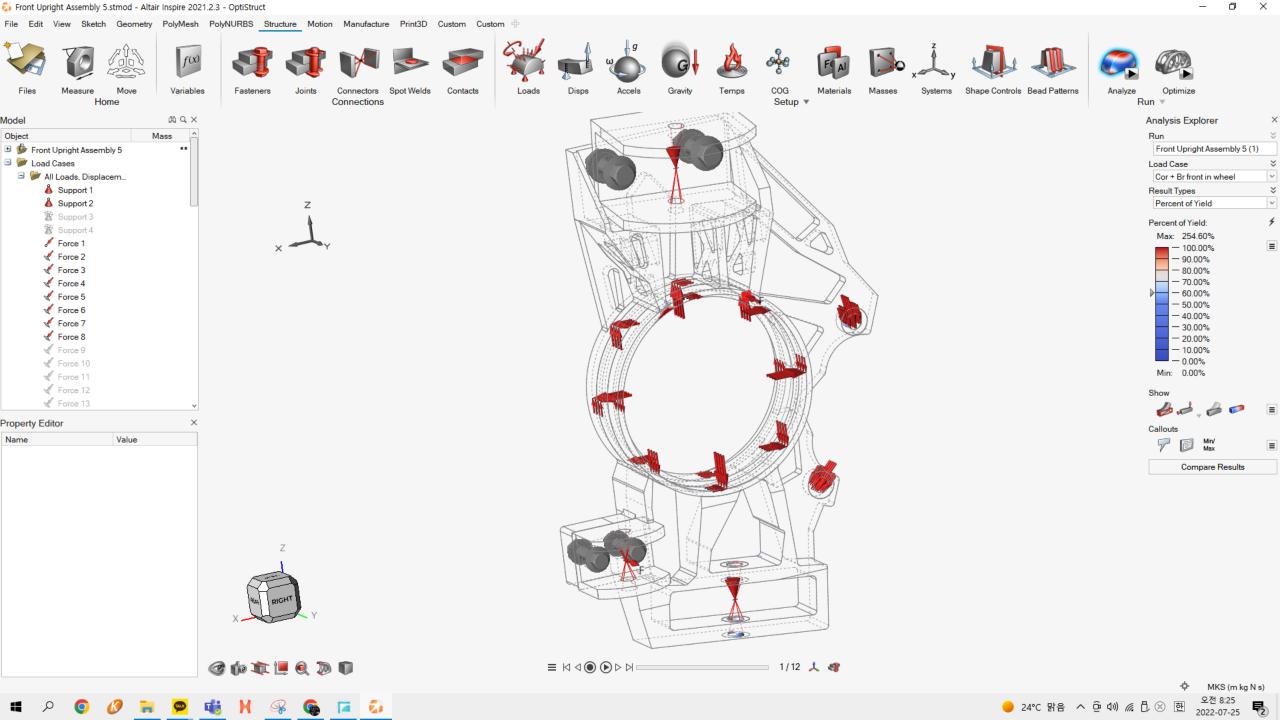






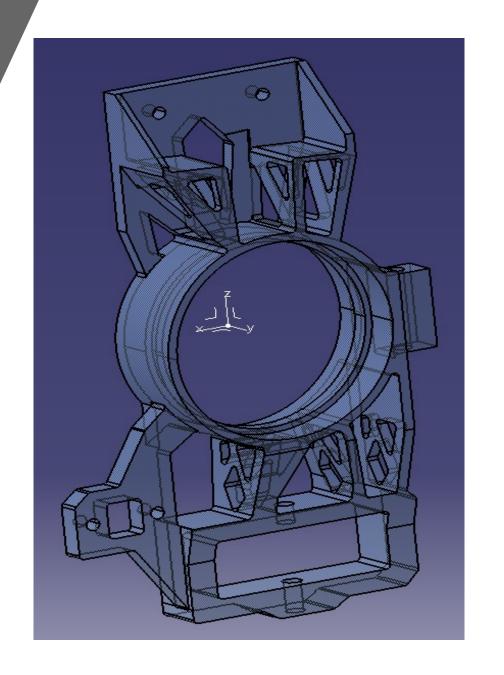


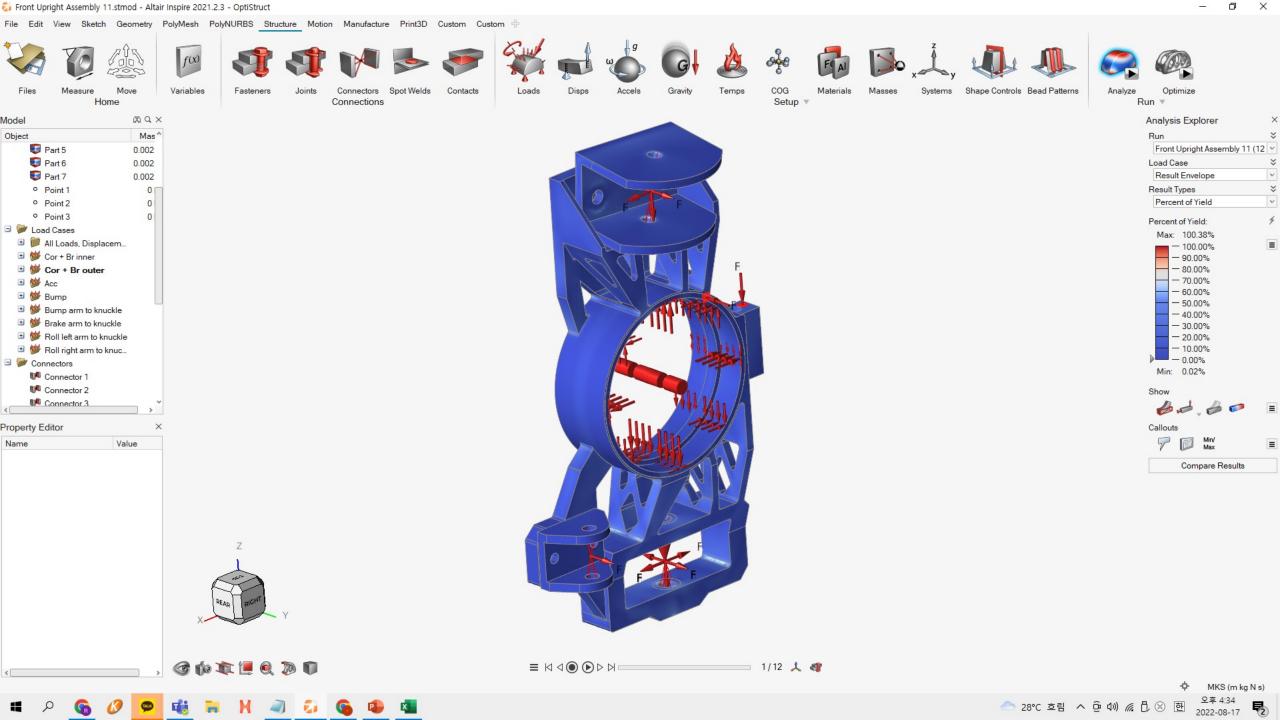


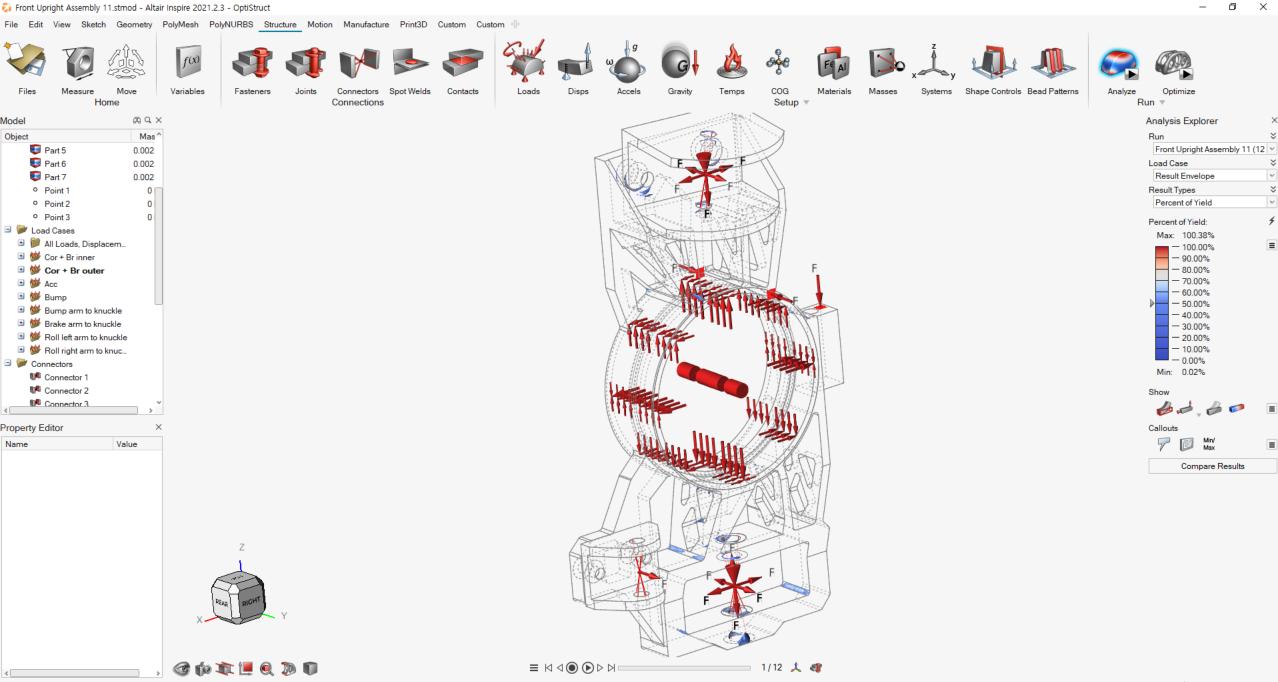


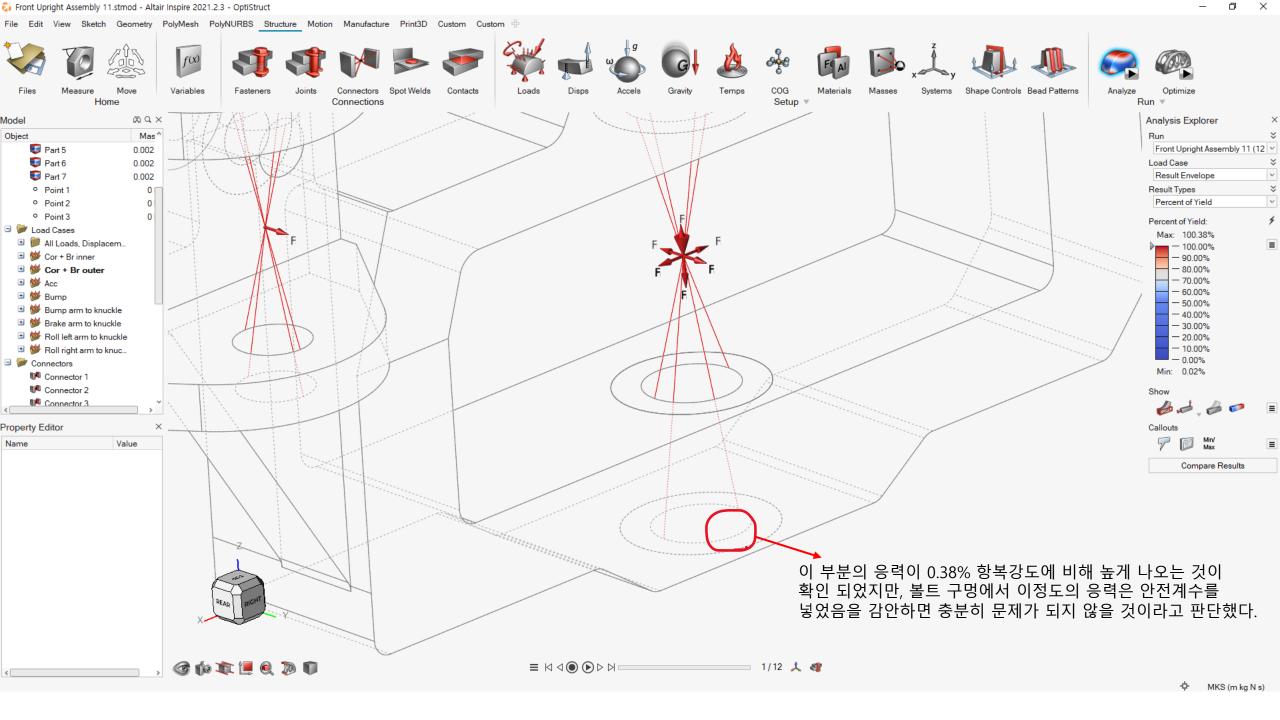
캘리퍼의 마운트 부분의 응력이 항복강도보다 높음, 구조상 그 부분의 두께를 늘릴 수 없는 상황.

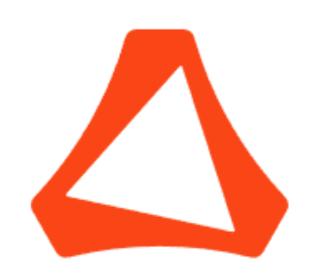
->마운트 형상을 다른 방식으로 수정, 캘리퍼의 모델을 바꾸어서 설계.







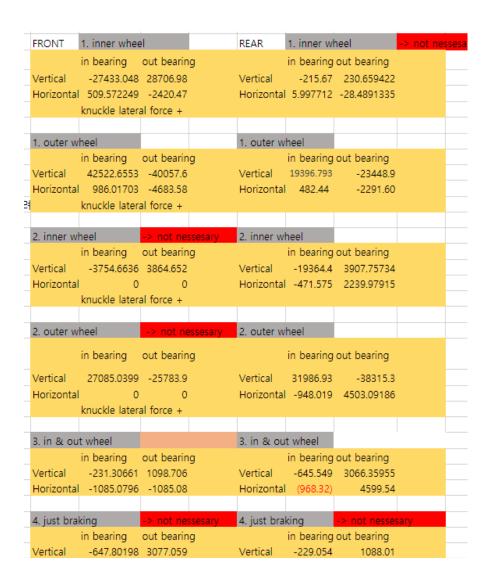




해석결과 및 한계

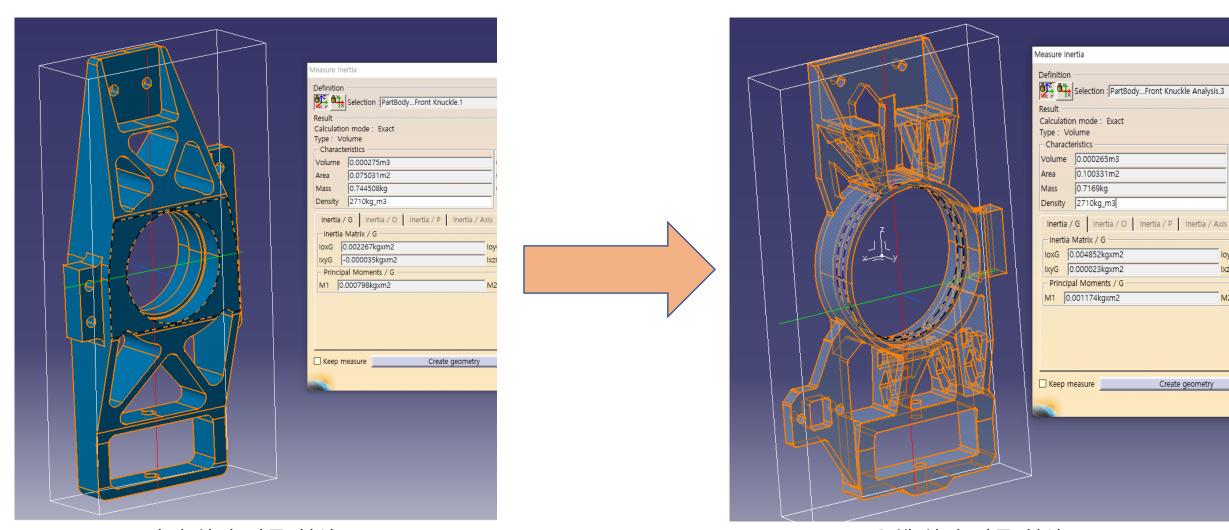
FRONT	1. inner whee	l		REAR	1. inner wh	neel	-> not nes
	in bearing	out bearing	9		in bearing	out bearing	
Vertical	-16286.833	17185.4		Vertical	-347.81	529.383157	
Horizontal	617.749587	-1965.57	•	Horizontal	124.834	-397.19974	
	knuckle latera	I force +					
1. outer wheel				1. outer wheel			
	in bearing	out bearing	9			out bearing	
Vertical	24634.5556	-22964.5		Vertical	9723.1659	-13426.7	
Horizontal	1148.16658	-3653.26		Horizontal	655.25	-2084.89	
	knuckle latera	l force +					
2. inner wh	neel	-> not nes	sesary	2. inner wh	neel		
	in bearing	out bearing	9		in bearing	out bearing	
Vertical	-2183.47	2329.22		Vertical	-10588.3	3907.75734	
Horizontal	0	0		Horizontal	-642.379	2043.93272	
	knuckle latera	I force +					
2. outer wh	heel	-> not ne	ssesary	2. outer wh	heel		
	neel in bearing					out bearing	
		out bearing	9		in bearing	out bearing -24605.6	
	in bearing 15454.5854	out bearing	9	Vertical	in bearing 17796.4	_	
Vertical	in bearing 15454.5854	out bearing -14537.3 0	9	Vertical	in bearing 17796.4	-24605.6	
Vertical	in bearing 15454.5854 0	out bearing -14537.3 0	9	Vertical	in bearing 17796.4	-24605.6	
Vertical	in bearing 15454.5854 0 knuckle latera	out bearing -14537.3 0	9	Vertical	in bearing 17796.4 -1172.8	-24605.6	
Vertical Horizontal 3. in & out	in bearing 15454.5854 0 knuckle latera	out bearing -14537.3 0 I force +	9	Vertical Horizontal 3. in & out	in bearing 17796.4 -1172.8 t wheel	-24605.6	
Vertical Horizontal 3. in & out	in bearing 15454.5854 0 knuckle latera t wheel	out bearing -14537.3 0 I force +	9	Vertical Horizontal 3. in & out	in bearing 17796.4 -1172.8 t wheel in bearing	-24605.6 3731.62315	
Vertical Horizontal 3. in & out	in bearing 15454.5854 0 knuckle latera t wheel in bearing	out bearing -14537.3 0 I force + out bearing -887.514	9	Vertical Horizontal 3. in & out Vertical	in bearing 17796.4 -1172.8 t wheel in bearing -1127.6	-24605.6 3731.62315 out bearing	
Vertical Horizontal 3. in & out Vertical Horizontal	in bearing 15454.5854 0 knuckle latera t wheel in bearing 278.932885 -829.5336	out bearing -14537.3 0 I force + out bearing -887.514	9	Vertical Horizontal 3. in & out Vertical	in bearing 17796.4 -1172.8 t wheel in bearing -1127.6	-24605.6 3731.62315 out bearing 3587.81841	
Vertical Horizontal 3. in & out Vertical Horizontal	in bearing 15454.5854 0 knuckle latera t wheel in bearing 278.932885	out bearing -14537.3 0 I force + out bearing -887.514	9	Vertical Horizontal 3. in & out Vertical Horizontal 4. just brak	in bearing 17796.4 -1172.8 t wheel in bearing -1127.6 (1691.40)	-24605.6 3731.62315 out bearing 3587.81841 5381.73	ary
Vertical Horizontal 3. in & out Vertical Horizontal 4. just brak	in bearing 15454.5854 0 knuckle latera t wheel in bearing 278.932885 -829.5336	out bearing -14537.3 0 I force + out bearing -887.514 -829.534	g g sesary	Vertical Horizontal 3. in & out Vertical Horizontal 4. just brak	in bearing 17796.4 -1172.8 t wheel in bearing -1127.6 (1691.40)	-24605.6 3731.62315 out bearing 3587.81841 5381.73	агу
Vertical Horizontal 3. in & our Vertical Horizontal 4. just brak	in bearing 15454.5854 0 knuckle latera t wheel in bearing 278.932885 -829.5336	out bearing -14537.3 0 I force + out bearing -887.514 -829.534 -> not nes out bearing	g sesary	Vertical Horizontal 3. in & out Vertical Horizontal 4. just brak	in bearing 17796.4 -1172.8 t wheel in bearing -1127.6 (1691.40) king in bearing	-24605.6 3731.62315 out bearing 3587.81841 5381.73	ery
Vertical Horizontal 3. in & out Vertical Horizontal 4. just brak Vertical	in bearing 15454.5854 0 knuckle latera t wheel in bearing 278.932885 -829.5336 king in bearing	out bearing -14537.3 0 I force + out bearing -887.514 -829.534 -> not nes out bearing 604.921	sesary	Vertical Horizontal 3. in & out Vertical Horizontal 4. just brak Vertical	in bearing 17796.4 -1172.8 t wheel in bearing -1127.6 (1691.40) cing in bearing -658.549	-24605.6 3731.62315 out bearing 3587.81841 5381.73 -> not nesses out bearing	ary

<작년 차량의 너클 하중>



<올해 차량의 너클 하중>

에어로 파츠 장착 및 모터 성능 향상, Maximum speed Target값 등의 향상으로 너클의 설계 하중이 작년 차량보다 각 상황별로 적게는 2~30% 많게는 7~80% 증가하였다.



<작년 차량 너클 형상>

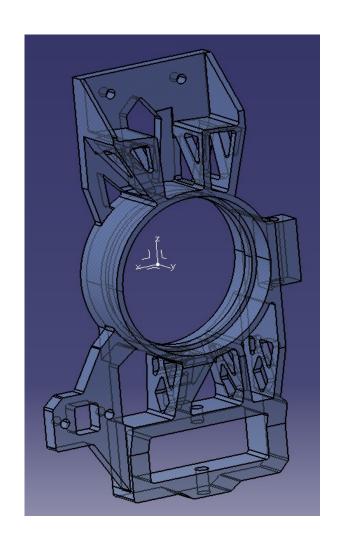
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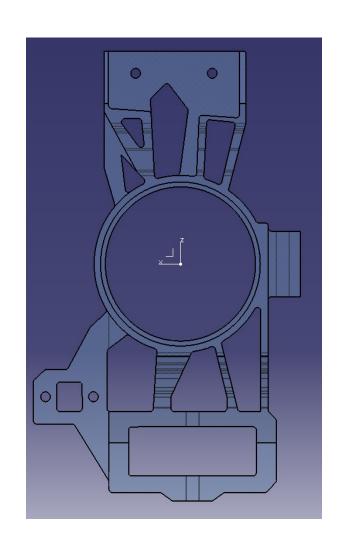
0.100331m2

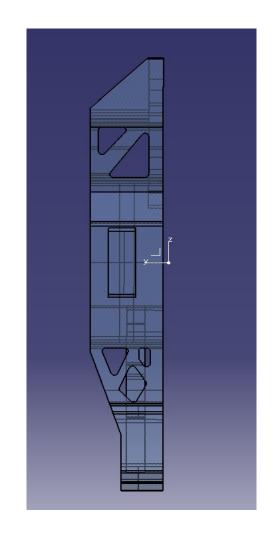
0.7169kg

질량이 0.7445kg 에서 0.7169kg 으로 약 3.7% 감량하였다.

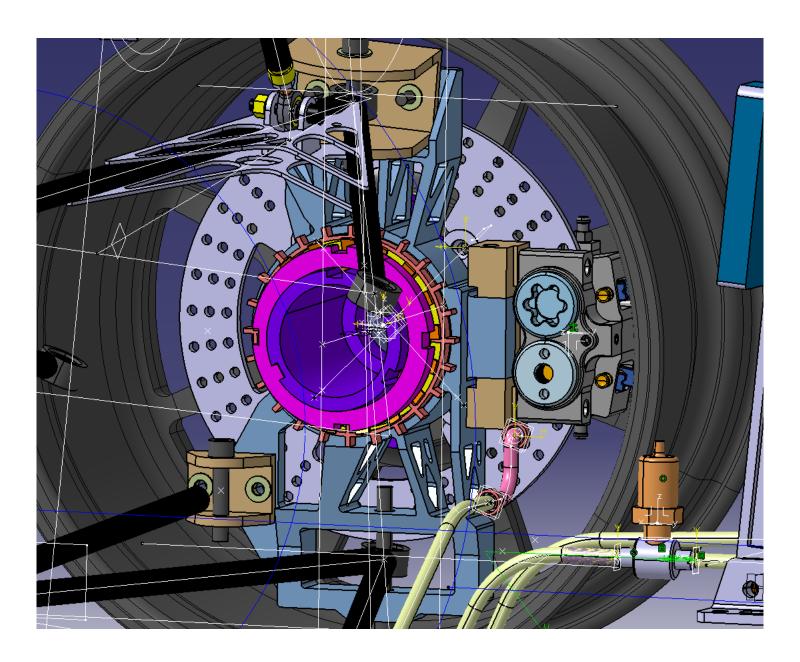
<너클 최종 형상 및 어셈블리>







<너클 최종 형상 및 어셈블리>





<한계 및 앞으로의 과제>

- 1. CNC 가공의 형상을 고려하다 보니, 생각보다 아쉬운 질량 감량 효과.
- 2. 볼트 구멍 부분의 응력집중현상.
- -> Hyperworks 에서 메쉬 형상 수정을 통한 더블체크

서스펜션 벨 크랭크 최적설계

서스펜션 부품 최적화 진행

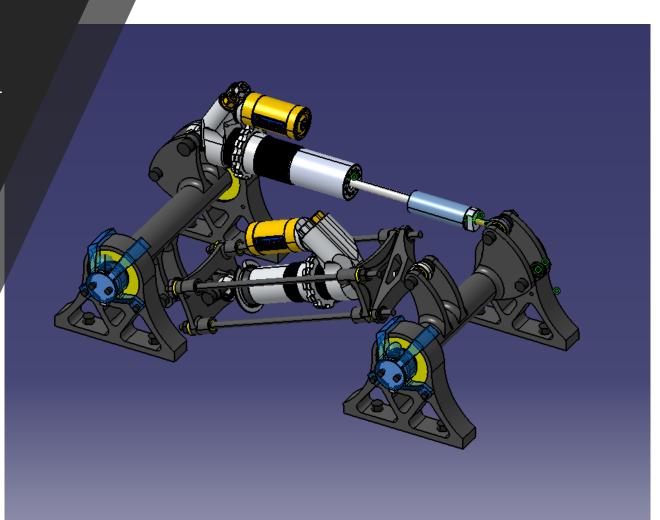
- 타이어의 거동에 중요한 현가 하 질량의 경량화
- 늘어난 차량 스펙에 따른 부품 경량화 필수

벨 크랭크 최적화 진행

- 현가 하 질량으로만 이루어져 있음
- 형상의 다양성이 무궁무진

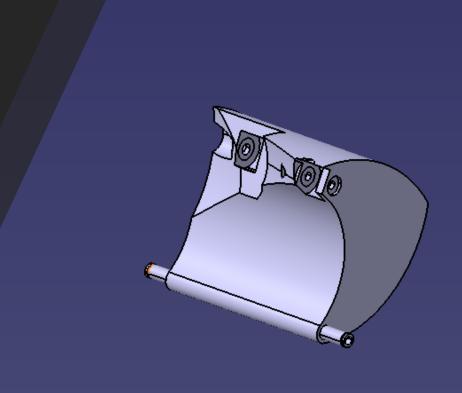
제작 계획

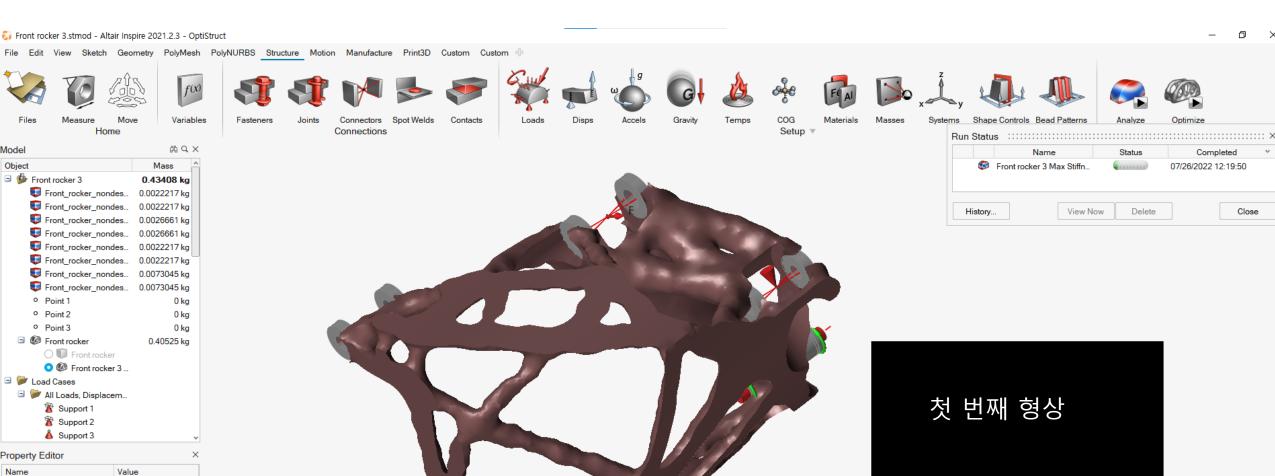
- 티타늄 합금 금속 3D 프린팅 (레이저 소결식)

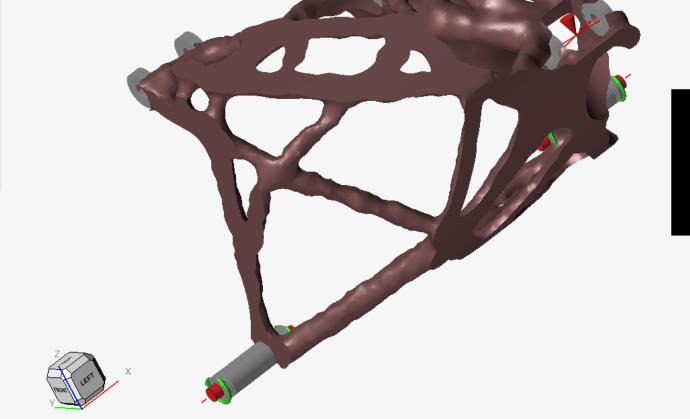


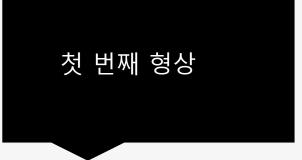
서스펜션 벨 크랭크 최적설계

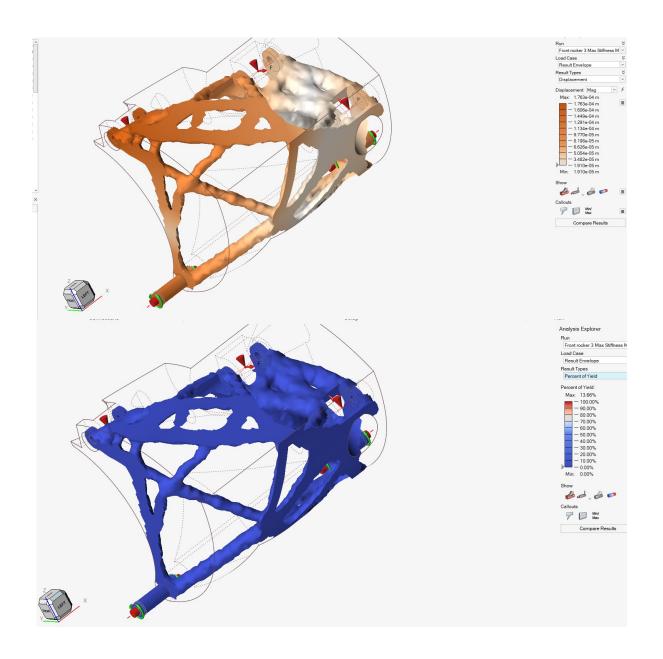
- 첫 번째 디자인 스페이스 설정 댐퍼, 가변저항 마운트를 위한 공간 벨 크랭크의 피벗 축을 위한 공간





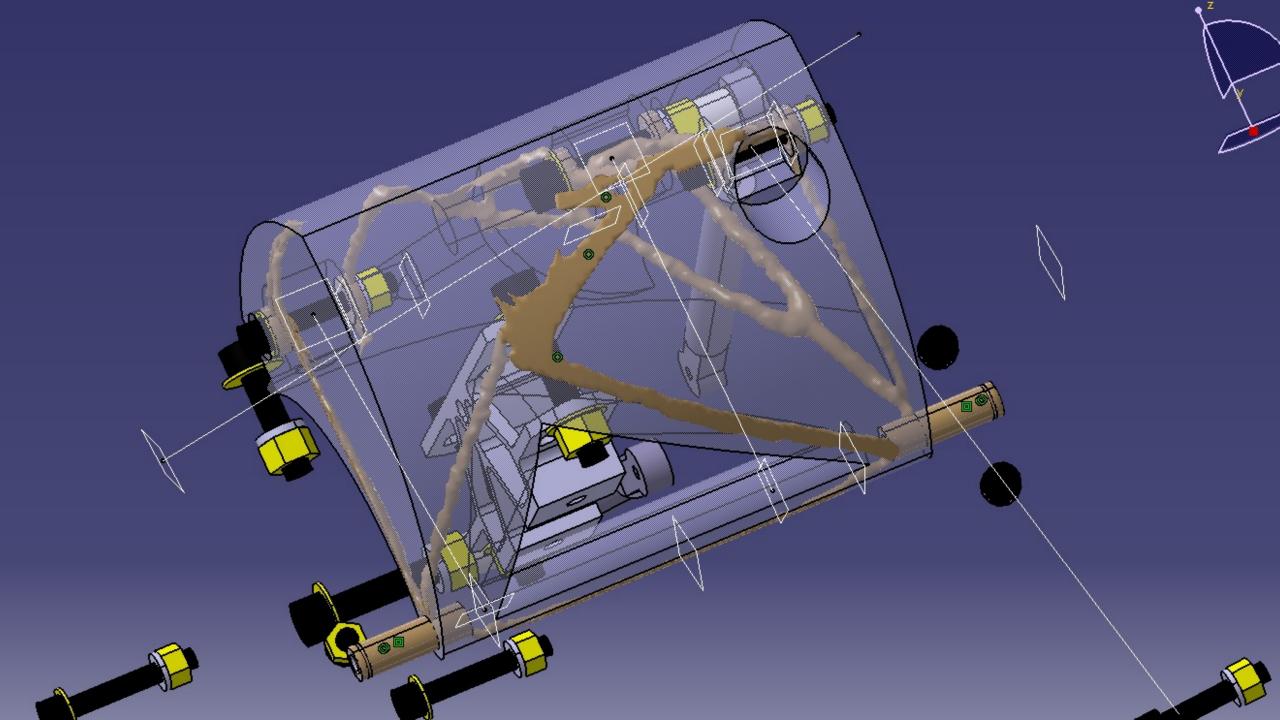


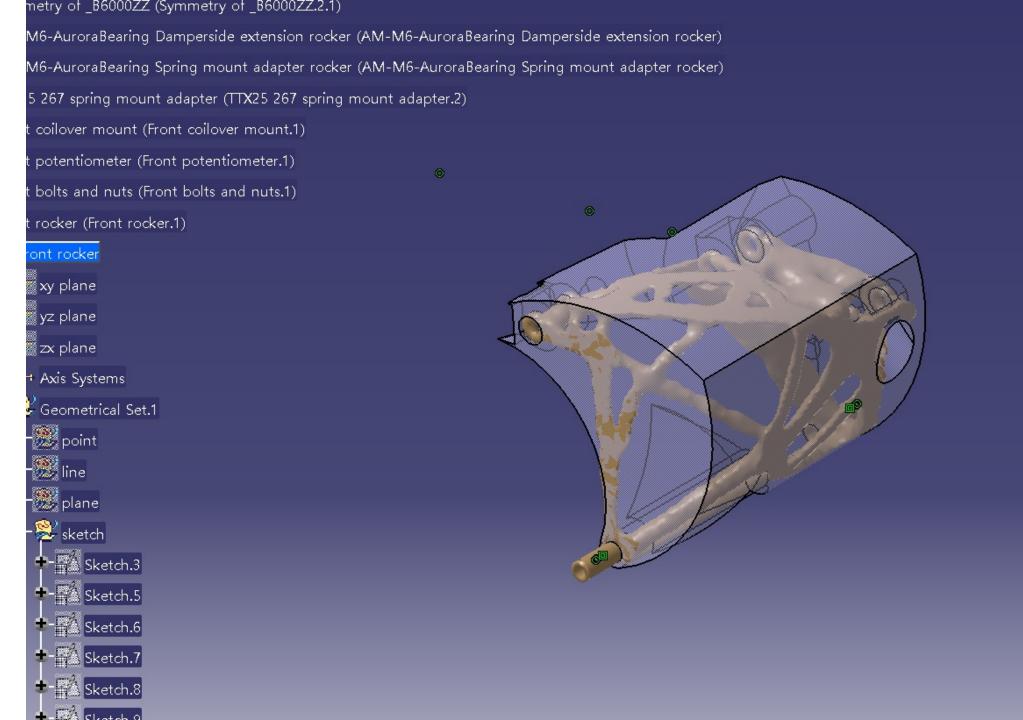


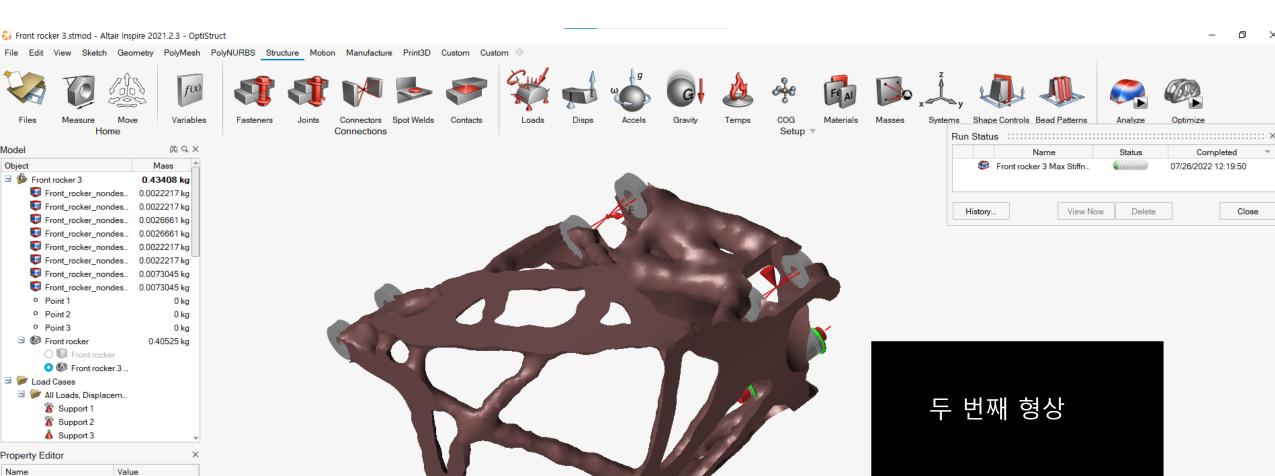


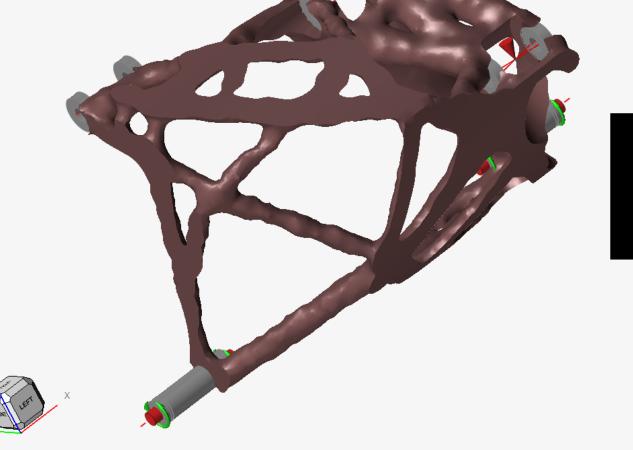
첫 번째 형상 해석 결과 두 번째 디자인 스페이스 설정

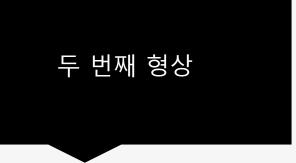
- 부재의 두께만 변한다고 상정
- Minimum thickness 재설정
- 부재가 부족한 부분과 과한 부분 판단

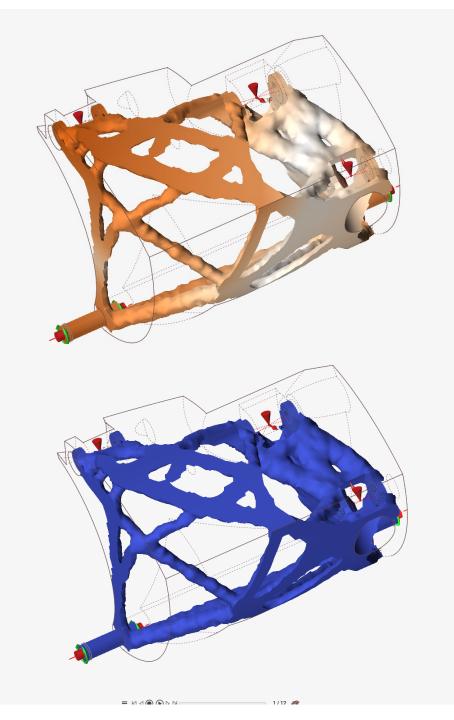




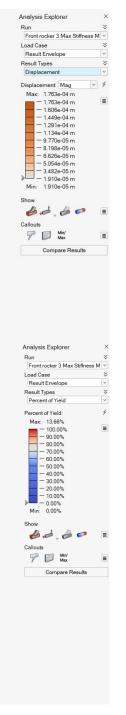






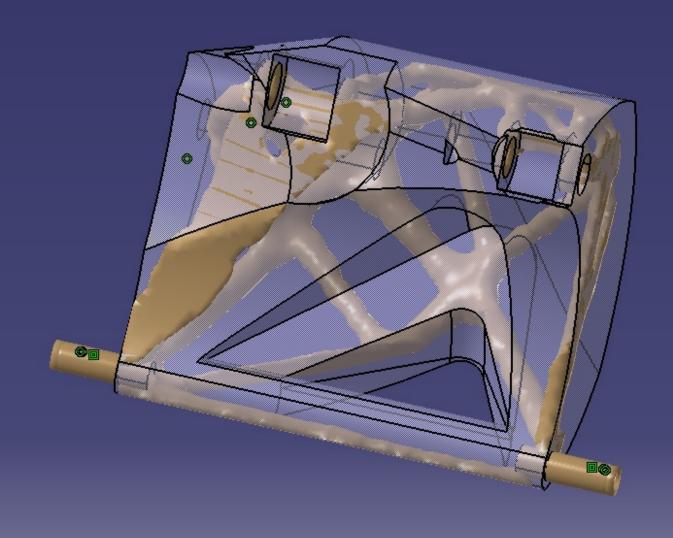


750



두 번째 형상 해석 결과 세 번째 디자인 스페이스 설정

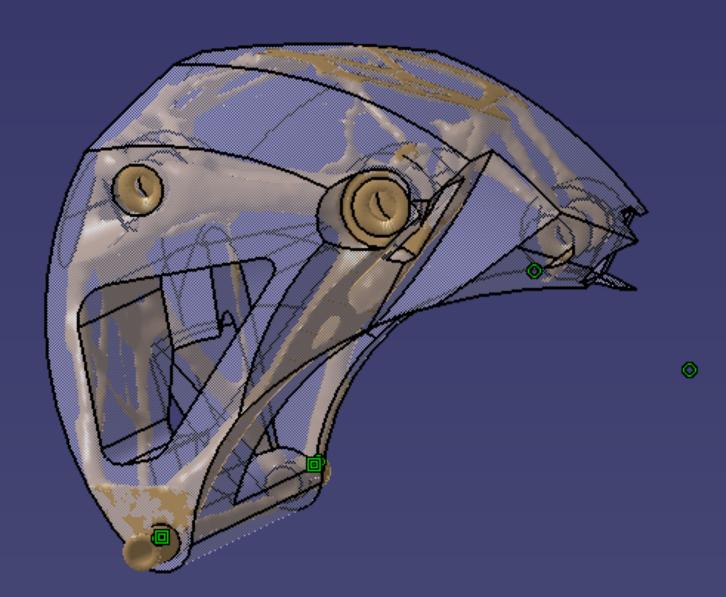
- Minimum thickness 재설정
- 피벗 축의 바깥 쪽 부재 추가



sign space

ace

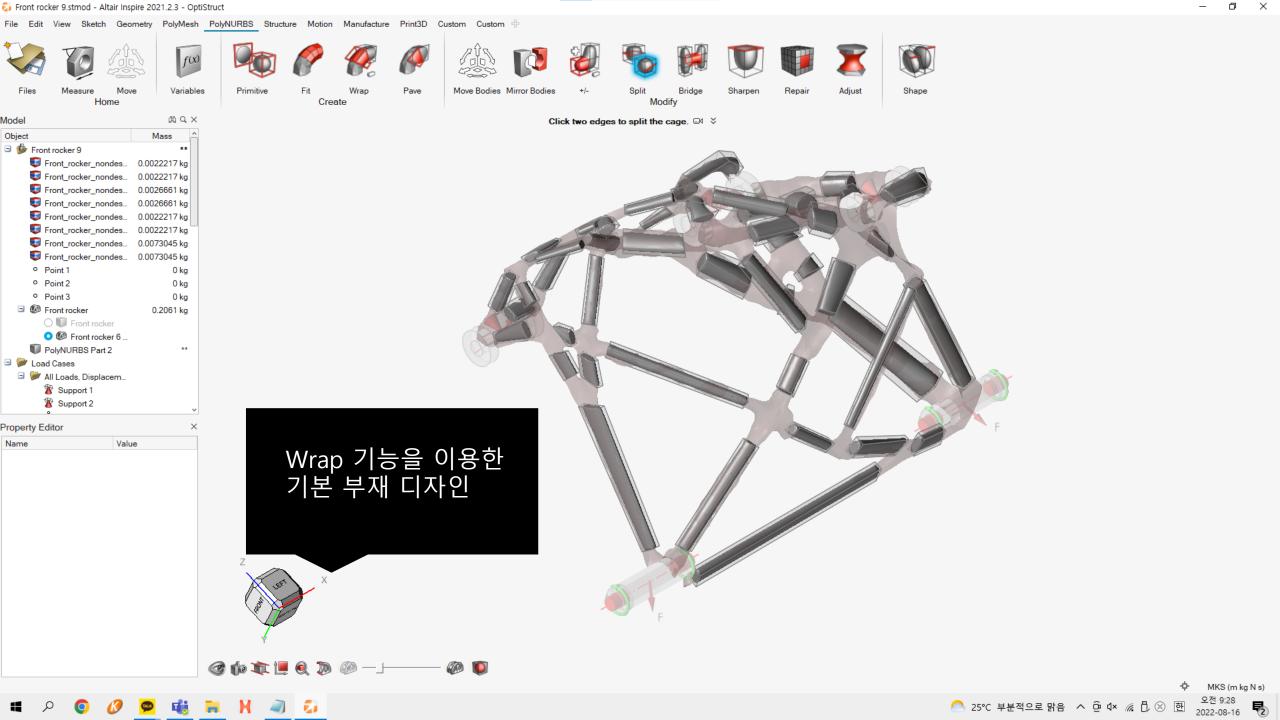
n_space

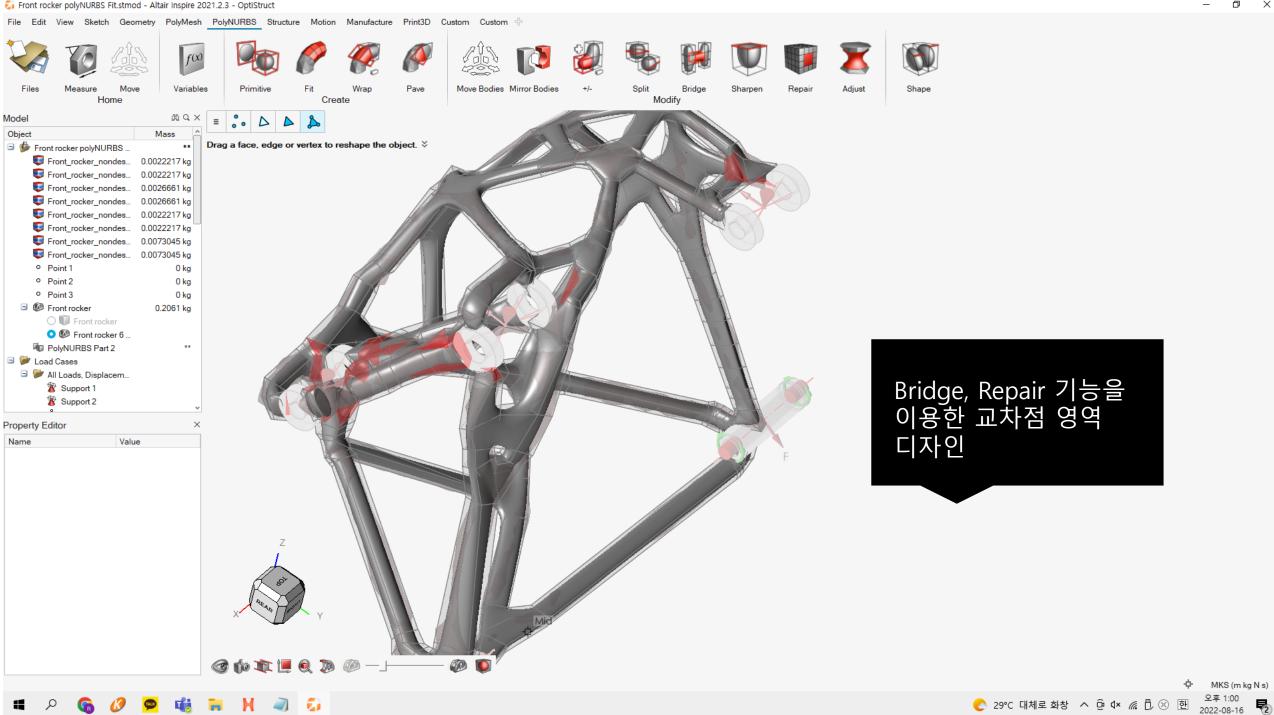


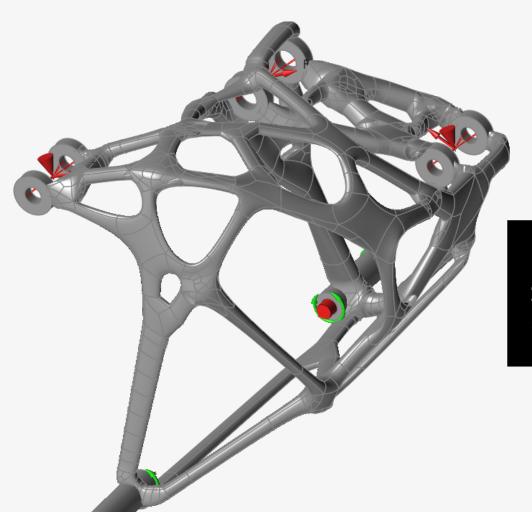
서스펜션 벨 크랭크 최적설계

제작을 위한 설계 후 처리

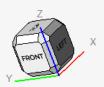
- 세 번째 최적화 형상을 바탕으로 한
- polyNURBS 기능 사용 응력 집중을 최대한 피하고, 기존의 Nondesign space를 침범하지 않게끔 디자인



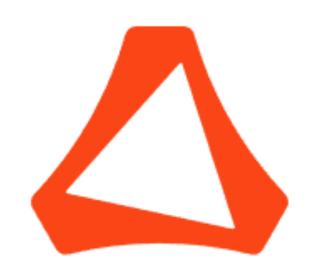




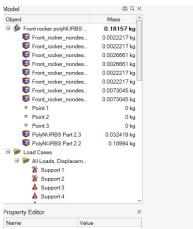
Repair 등을 이용한 Surface 모델 수정 후 최종 Solid 모델 형상

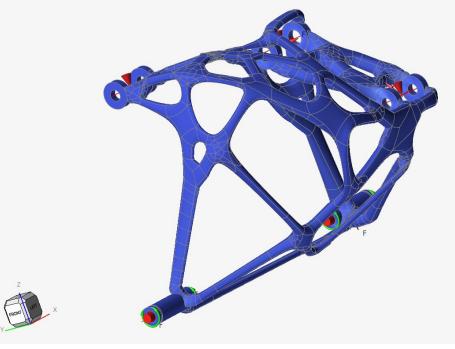


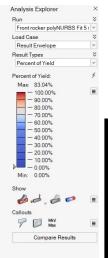




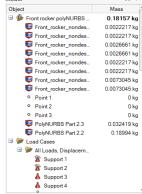
해석결과 및 작년 차량과의 비교



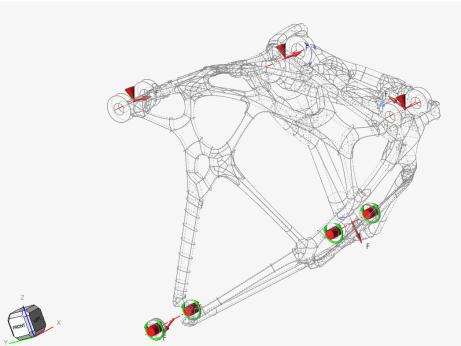


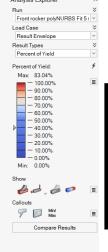


Result envelope에서 최대 응력이 항복 강도 의 83.54%

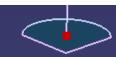


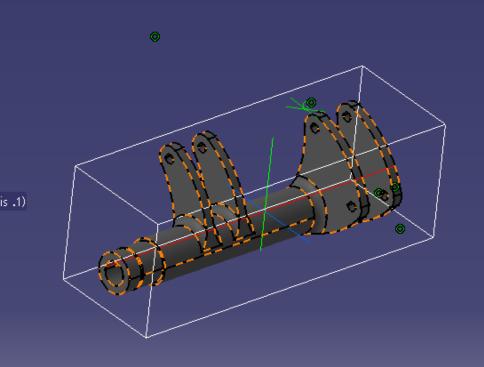
a d	Support 3		
	& Support 4		
roperty Ed	itor		
Name		Value	



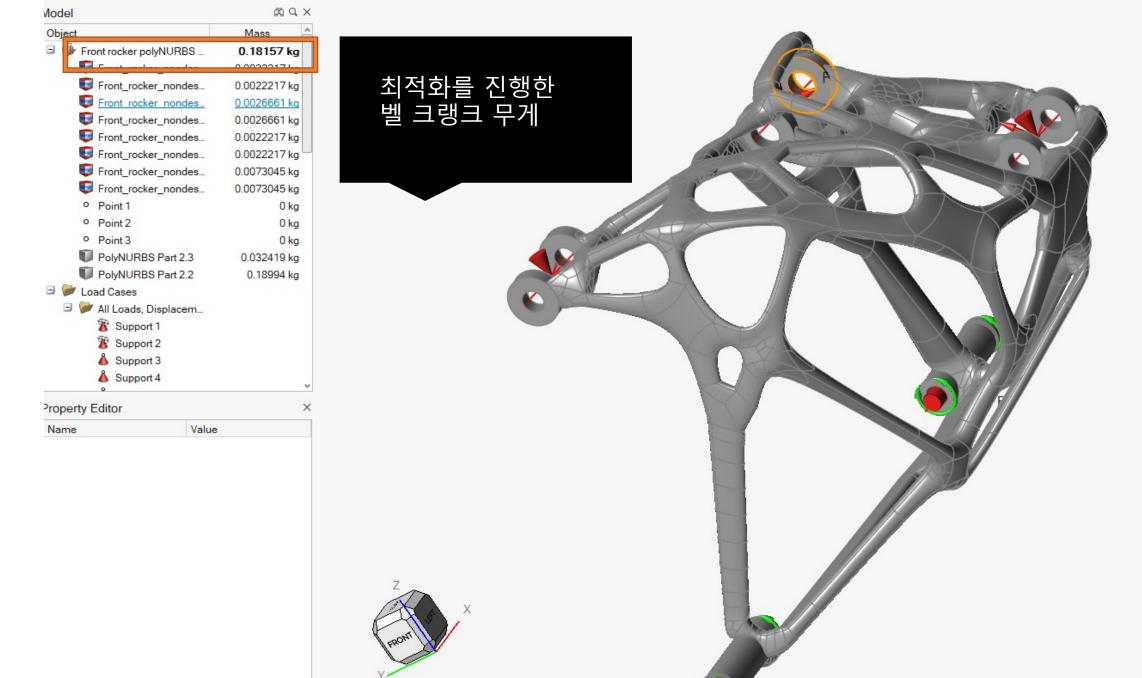


대부분의 부재에서 받 는 응력이 항복 강도의 50%를 밑도는 모습

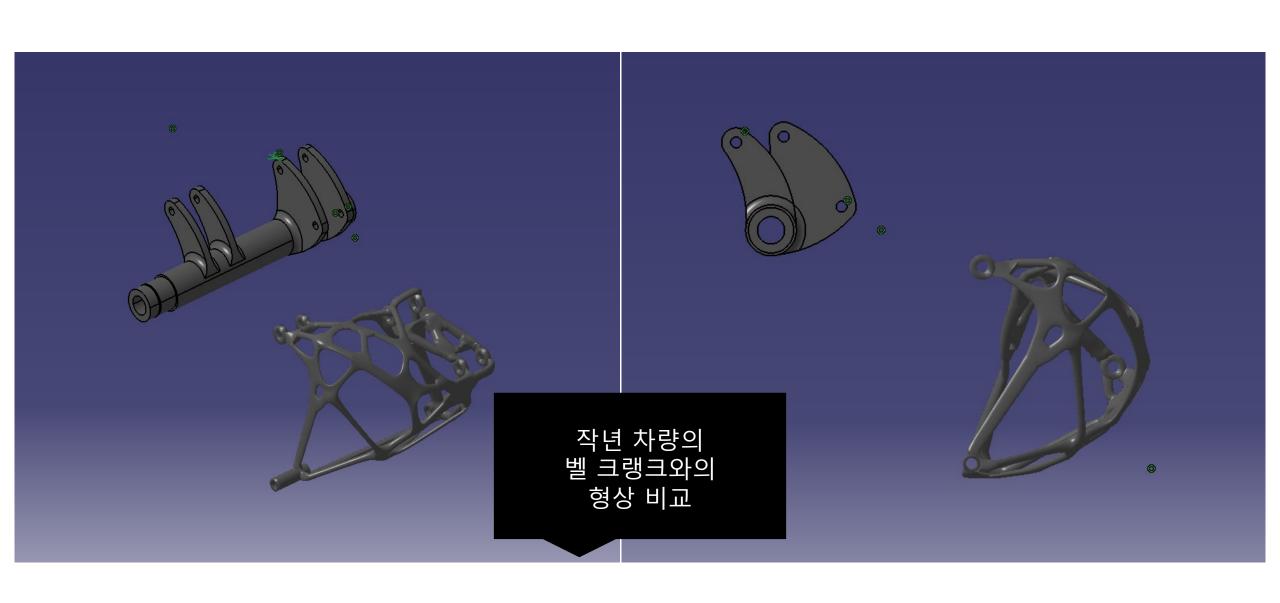




Measure Inertia		? >
Definition Selection: left rodFront Suspension Rocke	r Axis .1	
Result Calculation mode: Exact Type: Volume Characteristics Volume 1.272e-004m3 Area 0.045m2 Mass 0.345kg	Center Of Gravity (6 Gx -41.431mm Gy -148.446mm 벨 크랭크 무게	
Density Priorg_ms		
Inertia / G Inertia / O Inertia / P Inertia / A	xis Inertia / Axis System	
Inertia Matrix / G		
loxG 1.444e-004kgxm2	loyG 0.001 kgxm2 lozG 0.001 kg	:gxm2
lxyG 8.186e-005kgxm2	lxzG -4.764e-005kgxm2 lyzG 1.05e-	005kgxm2
Principal Moments / G		
M1 1.356e-004kgxm2	M2 0.001kgxm2 M3 0.001kg	jxm2
☐ Keep measure Create geometry	Export	Customize
		OK Canc



A 10 10 10 10



서스펜션 벨 크랭크 최적설계



<결과>

작년 차량보다 벨 크랭크가 받는 하중과 모멘트 암 증가 그러나 345g에서 182g으로 47.3% 경량화 성공

재료가 AI 6061에서 Titanium 6AI4V 로 바뀌었다. 티타늄 합금이 질량 대비 강성이 2배 가량 좋은 것을 생각하면 동일한 하중과 동일한 모멘트 암일 때 50% 경량화 되어야 한다는 점이 자연스럽다. 하지만 무게를 두배 정도 증가시키는 요인들이 있음에도 50% 가량을 경량화 하였다는 점을 생각하면 최적화 효율이 굉장하다고 생각할 수 있다.



감사합니다.

한양대학교 자작자동차동아리 팀 RACE -김범수, 민동혁



Q&A

한양대학교 자작자동차동아리 팀 RACE -김범수, 민동혁